416 Rec'd PCT/PTO 1 7 APR 2000

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TRANSMITTAL LETTER	TO THE UNITED STATES	Mo-5599/LeA 32,647
	ED OFFICE (DO/EO/US)	U.S. APPLICATION NO (II kmm a sec 17 CLR LS)
	4G UNDER 35 U.S.C. 371	то ве 0.9 г/т 29680
WITERNATIONAL APPLICATION NO	INTERNATIONAL FILING DATE	PRIORITY DATE CLAIMED
PCT/EP98/06375	October 7, 1998	October 20, 1997
ITHE OF INVENTION	Them and Use of the Same	
~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~	ntaining Sintering Additives a	nd SiO <sub>2</sub> , Method For Producing
APPLICANT(S) FOR DO/FO/US Gerhard Wotting, Mathias Herro	nann, Grit Michael, Stefan Sie	gel, Lutz Frassek
		3) the following items and other information
t. X This is a LIRST submission of item	ns concerning a filing under 35 U.S.C. 371	
2. This is a SECOND or SUBSEQUE	ENT submission of items concerning a filing	under 35 t/ S C 371
3. K This express request to begin natio	nal examination procedures (35 U S C 371(	(i) at any time rather than delay
	the applicable time limit set in 35 USC 37	-
4. X A proper Demand for International	Preliminary Examination was made by the 19	h month from the earliest claimed priority date
5. X A copy of the International Applic	ation as filed (35 U S C 371(c)(2))	
a 🗓 is transmitted herewith (	required only if not transmitted by the Interi	ational Burcau)
b. has been transmitted by	the International Bureau	
c. Is not required, as the ap	oplication was filed in the United States Reco	erving Office (RO/US)
6. XIA translation of the International	Application into English (35 U.S.C. 371(c))	2))
7. Amendments to the claims of the	International Aplication under PC1 Article	19 (35 U.S.C. 371(c)(3))
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	by the International Bureau	
have not been made, he	owever, the time limit for making such amen	dments has NOT expired
have not been made an	d will not be made	
8. $\prod_{i=1}^{n-1} A$ translation of the amendments	to the claims under PCT Article 19 (35 U.S.	C 371(c)(3))
9. X n oath or declaration of the inv	rentor(s) (35 U.S.C. 371(c)(4)).	
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16. [X] Other items or information	Abstract; Drawings (Figures 1 Notification of the Recording	& 2) of a Change

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PATENT APPLICATION Mo-5599 LeA 32,647

# IN THE UNITED STATES PATENT AND TRADEMARK OFFICE

APPLICA	ATION OF	)
GERHAF	RD WÖTTING ET AL	) PCT/EP98/06375 )
SERIAL	NUMBER: TO BE ASSIGNED	) )
FILED:	HEREWITH	) )
TITLE:	SILICON NITRIDE SUBSTANCES CONTAINING SINTERING ADDI- TIVES AND SIO <sub>2</sub> , METHOD FOR PRODUCING THEM AND USE OF THE SAME	) ) ) )

## PRELIMINARY AMENDMENT

Assistant Commissioner for Patents

Washington, D.C. 20231

Sir:

Applicants respectfully request entry of the following amendments prior to examination of the above-mentioned patent application.

### IN THE CLAIMS:

- 1. (Amended) Silicon nitride materials containing sintering aids and SiO<sub>2</sub> and a grain boundary phase, [characterized in that] wherein the molar ratio of the silicon dioxide in the grain boundary phase to the sintering additives including SiO<sub>2</sub> in the grain boundary phase is >60% and the oxide nitride content <1%.
- 2. (Amended) <u>A process</u> [Process] for producing silicon nitride materials [according to Claim 1, characterized in that] <u>wherein</u>, either alone or in combination,

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- a) the Si<sub>3</sub>N<sub>4</sub> powder used, either alone or together with the sintering aids, is thermally oxidized,
- b) the Si<sub>3</sub>N<sub>4</sub> powder, either alone or together with the sintering aids and, if desired, further additives, is tribooxidized during milling and/or
- the Si<sub>3</sub>N<sub>4</sub> powder is admixed with sintering aids or with SiO<sub>2</sub> or at least one SiO<sub>2</sub>-forming component either before or during milling[.] wherein the silicon nitride materials contain sintering aids and SiO<sub>2</sub>, and a grain boundary phase in which the molar ratio of the silicon dioxide in the grain boundary phase to the sintering additives including SiO<sub>2</sub> in the grain boundary phase is >60% and the oxide nitride content <1%.

Please delete Claim 3.

#### IN THE SPECIFICATION:

In the title, delete the title and insert --SILICON NITRIDE SUBSTANCES CONTAINING SINTERING ADDITIVES AND SiO<sub>2</sub>, METHOD FOR PRODUCING THEM AND USE OF THE SAME--.

At page 1, below the title, please add:

--BACKGROUND OF THE INVENTION--.

At page 2, above line 15, please add:

-- DESCRIPTION OF THE INVENTION ---.

At page 5, line 31, after "character," please add:

--All parts and percentages are by weight unless otherwise indicated.--

At page 8, below line 22, please add:

--Although the present invention has been described in detail with reference to certain preferred versions thereof, other variations are possible. Therefore, the spirit and scope of the appended claims should not be limited to the description of the versions contained therein.--

Please add the following Abstract, submitted herein separately:

Mo-5599 - 2 -

# --SILICON NITRIDE SUBSTANCES CONTAINING SINTERING ADDITIVES AND SiO<sub>2</sub>, METHOD FOR PRODUCING THEM AND USE OF THE SAME

### ABSTRACT OF THE DISCLOSURE

The invention relates to silicon nitride substances containing sintering additives and SiO<sub>2</sub>, a method for producing them and the use of the same.--

#### **REMARKS**

Entry of this Preliminary Amendment is requested. The amendments made above have been made to place the application in conformance with American patent practice. No new matter has been added. Claim 3 was deleted.

Respectfully submitted,

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PCT/EP98/06375

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Silicon nitride materials containing sintering aids and SiO2, a process for producing them and their use

The present invention relates to silicon nitride materials containing sintering aids and SiO<sub>2</sub>, a process for producing them and their use.

Ceramic materials are finding ever wider use in the construction of machinery and apparatus, in particular in bearings (Ceramic Airframe Bearings: Lubrications Engeneering, 31 (1975), 558-564). All-ceramic bearings have proven useful particularly in applications where there is little lubrication and in corrosive media. However, it has been found in a wide variety of application areas for components made of high-performance ceramic that they degrade and that their life cannot be reliably predicted. The corrosion resistance is dependent to a considerable extent on the type of corrosive medium, the material composition and the superposed mechanical stress. The cause of this is the different reaction behaviour of the individual components of the microstructure of the ceramics (matrix grains, grain boundary phases, impurities) towards acids, bases or under hydrothermal conditions. Liquid-phase-sintered materials such as silicon nitride or silicon carbide (LPSSIC) which contain from 5 to 20% by volume of grain boundary phases display attack along the grain boundary phase in acids and bases. In general, the main point of attack in acid and alkali corrosion in the temperature range <180°C is the grain boundary phase. However, this is not leached out entirely, which is made clear by materials which are corroded through to the centre still having strengths of from 300 to 400 MPa.

The corrosion rates for corrosion in the acid range are strongly dependent on the material composition. EP-A 649 824 discloses that MgO/Al<sub>2</sub>O<sub>3</sub>-containing materials have good acid resistance without the cause of this behaviour being completely known. One way of further improving the acid resistance of silicon nitride materials containing rare earth metal oxides, Y2O3 and possibly Al2O3 as sintering aids is to reduce the amount of these sintering aids. However, the resulting improvement in the

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Signature of person mailing paper or tee)

corrosion resistance has to be bought by higher manufacturing costs, since HIP technology is required for densification (EP-A 414 383). Furthermore, Mater. Res. Soc. Symp. Proc. 287 (1993) and Key Engeneering Materials 113 (1996), pp. 227-237, report that corrosion is reduced at very high concentrations of acids, which in the case of phosphoric acid could be explained by formation of a passive layer, see Corrosion of High Performance Ceramics; Springer Verlag, Berlin, 1992; pp. 76 to 78.

There is therefore a great need for acid-stable ceramic materials.

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It is therefore an object of the invention to provide ceramic materials based on Si<sub>3</sub>N<sub>4</sub> which have a high corrosion resistance, i.e., for example, a low mass change and low strength losses after acid treatment.

15 It has now been found that a silicon nitride material has, regardless of the way in which it is produced, a high corrosion resistance towards acids if it has a very high SiO<sub>2</sub> content and formation of silicon oxide nitride is avoided, i.e. if the molar ratio of the silicon dioxide in the grain boundary phase to the sintering aids including SiO2 in the grain boundary phase is >60% and the oxide nitride content (Si<sub>2</sub>N<sub>2</sub>O content) is <1%.

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The invention accordingly provides silicon nitride materials containing sintering aids and SiO<sub>2</sub> and having a molar ratio of the silicon dioxide in the grain boundary phase to the sintering aids including SiO<sub>2</sub> in the grain boundary phase is >60%, preferably >65%, and the oxide nitride content ( $SiO_2N_2O$ ) is <1%.

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For the purposes of the present invention, sintering aids are the added substances which form the liquid phase during sintering and remain in the grain boundary phase.

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The grain boundary phase in silicon nitride materials is formed by solidification of the liquid phase present during sintering. It contains the sintering additives, silicon

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dioxide and sometimes dissolved silicon nitride. Depending on the conditions of the thermal treatment (cooling rate, etc), it is amorphous or partially crystalline. In general, it wets the silicon nitride particles and forms a three-dimensional network.

Sintering aids present in the grain boundary phase for the purposes of the invention are preferably Y<sub>2</sub>O<sub>3</sub>, Sc<sub>2</sub>O<sub>3</sub>, rare earth metal oxides, alkaline earth metal oxides and Al<sub>2</sub>O<sub>3</sub>.

The amount of the added sintering aids +  $SiO_2$  is preferably selected so that the proportion of grain boundary phase in the sintered material is < 20% by volume, particularly preferably 0.1 - 17% by volume, very particularly preferably from 3 to 15% by volume.

In one embodiment of the invention, the silicon nitride materials contain further additives.

Such additives are, for example, reactive additives, i.e. ones which react with  $Si_3N_4$  and form  $SiO_2$ , for example  $TiO_2$ ,  $WO_3$  and/or  $MoO_3$ . Thus,  $TiO_2$ , for example, reacts to form TiN, while, for example,  $WO_3$  and  $MoO_3$  form silicides with simultaneous oxidation of  $Si_3N_4$  to  $SiO_2$ .

It is likewise possible to use additives which are retained as disperse phases, for example SiC, TiN, MoSi<sub>2</sub>, TiCN and/or HfO<sub>2</sub> or else additives which form mixed crystals with the Si<sub>3</sub>N<sub>4</sub>, for example AlN.

The additives which react with  $Si_3N_4$  and form  $SiO_2$  are preferably present in an amount of from 0 to 10 mol%, preferably <5 mol%, based on  $Si_3N_4$ .

The additives remaining as a disperse phase are preferably present in an amount of from 0 to 30% by volume.

Additives which form mixed crystals are preferably present in amounts of from 0 to 50 mol%, preferably <15 mol%, based on Si<sub>3</sub>N<sub>4</sub>.

In a preferred embodiment of the invention, the porosity of the material is <2%.

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The invention additionally provides a process for producing the material of the invention, in which, either alone or in combination,

- a) the Si<sub>3</sub>N<sub>4</sub> powder used, either alone or together with the sintering aids and, if
  desired, further additives, is thermally oxidized or
  - b) the Si<sub>3</sub>N<sub>4</sub> powder, either alone or together with the sintering aids and, if desired, further additives, is tribooxidized during milling or
- the Si<sub>3</sub>N<sub>4</sub> powder is admixed with sintering aids or with SiO<sub>2</sub> or at least one SiO<sub>2</sub>-forming component either before or during milling.

Any commercial  $Si_3N_4$  powder can be used for the processes according to a), b) and c).

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The thermal oxidation a) is carried out in an oxidizing atmosphere, preferably in air,  $O_2$  and/or water vapour at temperatures of from 300 to 1400°C. In the variant a), a milling step can also be carried out before or after the oxidation.

- The tribooxidation b) during milling is carried out by intensive milling of the Si<sub>3</sub>N<sub>4</sub> powder dry or in a liquid such as H<sub>2</sub>O or an organic solvent, e.g. acetone, hexane or alcohol.
- Milling is preferably carried out in ball mills and is continued until the milled  $Si_3N_4$ 30 has a mean particle size (d<sub>50</sub>), preferably measured by means of a Master Sizer S, of

< 2.5  $\mu$ m, preferably < 1  $\mu$ m, and has the required molar ratio of SiO<sub>2</sub> to sintering aids.

In the variant c), the SiO<sub>2</sub>-forming components used can be siloxanes, silanes, silicone resins (see Material Science and Technology Vol. 178, Processing of Ceramics, VCH, Weinheim, (1996) Part II, 4-47, DE-A 43 18 974, EP-A 0 412 428, or the reactive additives described, e.g. TiO<sub>2</sub>, WO<sub>3</sub> and MoO<sub>3</sub>.

The amount of SiO<sub>2</sub>-forming components is dependent on the desired SiO<sub>2</sub> content of the sintered body.

The production of the sintered material from the powder mixtures obtained according to the variants a), b) and/or c) is preferably carried out using generally customary ceramic technology.

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The incorporation of the sintering aids or the additives which form mixed crystals and/or  $SiO_2$  into the silicon nitride crystal lattice can also influence the ratio of  $SiO_2$  to the sintering aids. In this case, when determining the  $SiO_2$ /sintering aid ratio, the proportion of the original sintering aids or  $SiO_2$  has to be reduced by the proportion incorporated into the crystal lattice. This is of particular significance in the case of  $\alpha$ '- and  $\beta$ '-SiAlONs, e.g. according to the following equation:

z/2 SiO<sub>2</sub> + zAlN + (2-1/2 z) Si<sub>3</sub>N<sub>4</sub> 
$$\rightarrow$$
 Si<sub>6-z</sub>Al<sub>z</sub> O<sub>z</sub>N<sub>8-z</sub> where Z = O - 4.2

This has to be taken into account when calculating the amounts to be weighed out.

The invention additionally provides for the use of the materials of the invention in the construction of machinery and apparatus, in particular in bearings.

The following examples serve to illustrate the invention without having any limiting character.

#### **Examples**

#### Example 1

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Si<sub>3</sub>N<sub>4</sub> powder (Baysinid®, obtainable from Bayer AG), Y<sub>2</sub>O<sub>3</sub> (grade fine, obtainable from H.C. Starck) and Al<sub>2</sub>O<sub>3</sub> powder (AKP-50®, obtainable from Sumitomo) and TiO<sub>2</sub> (P25, obtainable from Degussa) are mixed in amounts corresponding to the composition indicated in Table 1, homogenized in a stirred ball mill in aqueous suspension for 3 hours, spray dried and pressed to form bodies having dimensions of 50 x 60 x 8 mm. The particle size (d<sub>50</sub>) of the mix after homogenization was 0.5 μm, measured by means of a Master Sizer S at pH 11.0. The bodies are baked out at 600°C for 1 hour in air. They are sintered under gas pressure at 1830°C and 50 bar of N<sub>2</sub> for 1.5 hours. The weight losses of the specimens were from <0.3 to 1.8%, depending on the TiO<sub>2</sub> content of the mix. The sintered specimens are cut into test bars and the surfaces were ground.

Mix 1 b was milled for 6 hours at a higher rotational speed in order to increase the oxygen content.

## 20 Example 2

This example was carried out using a method analogous to Example 1. The deviations are described below.

Examples 2a and 2b were prepared using a method analogous to Example 1b.

The sintering of Example 2a was carried out in a BN-coated graphite crucible in a BN powder bed. The weight loss was 1.8%. In Example 2b, the sample was sintered in an RBSN crucible. The weight loss was 0.2%.

In Example 2c, 1.5% of silicone resin was additionally used as binder. Examples 2e and 2f were produced from silicon nitride powder produced by the plasma method and having a surface area of 60 m<sup>2</sup>/g and an SiO<sub>2</sub> content of 8%. The specimens were hot pressed at 1800°C.

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### Example 3

The test specimens were produced using a method similar to Example 1. Densification was carried out by a sinter-HIP method, and the weight loss was reduced to < 1.5% by means of the RBSN crucible and a high sample volume/available volume ratio.

### Example 4

The test specimens were produced using a method analogous to Example 2.

#### Example 5

The test specimens were produced using a method analogous to Example 1, with sintering being carried out at 1800°C.

The respective results are listed in Table 1. By way of example, the mass losses of Examples 1-4 recorded in the corrosion resistance test are shown in Fig. 1.

The following measurement methods were employed for determining the data reported in Table 1:

Flexural test bars having dimensions of 3 x 4 x 50 mm were cut from the sintered bodies and used to determine the mechanical properties and the corrosion performance.

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The strength was determined by means of the 4-point method (support spacing: 20/40 mm).

The corrosion performance was determined in thermostated glass vessels using 1 N acid. The acid/solid ratio was >200 ml/10 g of specimen. The acid was changed every 100 hours. The mass loss of the specimens was determined by periodic weighing at defined time intervals (see  $\Delta m$  in Tab. 1). The specimens were rinsed with distilled water and dried before weighing.

The oxide nitride content was determined on the specimens by means of XRD measurements. This was carried out using  $CuK\alpha$  radiation. The quantitative determination was carried out by means of a Rietveld programme (Refine++). The detection limit was 0.8% by mass of  $Si_2N_2O$ .

The oxygen content was determined by the hot gas extraction method. The error was <0.1% by mass. The SiO<sub>2</sub> content was calculated from the oxygen content.

The porosity was determined in polished sections (prepared as described in Practical Metallography, 27 (1990, 503-513)) at a magnification of 1000 by means of automatic image analysis (Quantiment 570). The proportion by area of the pores in the polished section was taken as the proportion by volume. In parallel thereto, the density was determined by the Archimedes method, in accordance with EN 993-1.

<u>Table 1</u> Compositions and corrosion performance of the materials

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		(additive	+ βSi <sub>3</sub> N <sub>4</sub>			conditions			
		+ SiO <sub>2</sub> )	Oxide nitride						
		%lom	content %						
				Porosity	o4b		Δm(100h),	Δm(500h),	o4b, MPa
					MPa		mg/cm <sup>2</sup>	mg/cm <sup>2</sup>	(500h)
1a C	1a C 5Y <sub>2</sub> O <sub>3</sub> 2Al <sub>2</sub> O <sub>3</sub> 1 TiO <sub>2</sub>	45	0	<0.5	850	in HCI, 60°C	5.6	8.5	450
1b   I	1b I 5Y <sub>2</sub> O <sub>3</sub> 2Al <sub>2</sub> O <sub>3</sub> 1 TiO <sub>2</sub> +SiO <sub>2</sub>	65	0	<0.5	850		0.3	0.3	800
1c 1	1c I 5Y <sub>2</sub> O <sub>3</sub> 2Al <sub>2</sub> O <sub>3</sub> 5 TiO <sub>2</sub>	74	0	<0.5	825		0.24	0.26	750
1d C	5Y <sub>2</sub> O <sub>3</sub> 2Al <sub>2</sub> O <sub>3</sub> 7.5 TiO <sub>2</sub>	80.4	33	<0.5	800		7.5	9.5	550
2a   C	2a C 5Y2O3 3Al2O3	30	0	<0.5	800	in HCl, 60°C	10	16	450
2b   I	2b I 5Y <sub>2</sub> O <sub>3</sub> 3AI <sub>2</sub> O <sub>3</sub>	74	0	<0.5	820		0.2	0.2	750
2c   I	2c I 5Y <sub>2</sub> O <sub>3</sub> 3Al <sub>2</sub> O <sub>3</sub>	72	0	<0.5	800		0.21	0.23	730
2d C	2d C 5Y <sub>2</sub> O <sub>3</sub> 3Al <sub>2</sub> O <sub>3</sub>	30	0	<0.5	820	in H <sub>2</sub> SO <sub>4</sub> , 60°C	6		450
2e I	2e $1   5Y_2O_3 3Al_2O_3 + SiO_2$	63	0	<0.5	725		0.32	0.38	059
2f C	2f C $5Y_2O_3$ $3AI_2O_3 + SiO_2$	81	27	<0.5	765		2.2	8.3	530
3 I	I 5Y <sub>2</sub> O <sub>3</sub> 1.5 Al <sub>2</sub> O <sub>3</sub> + 0.5 TiO <sub>2</sub>	63	0	<0.5	800	in H <sub>2</sub> SO <sub>4</sub> , 60°C	0.35	0.5	200
4 C	C 3Y <sub>2</sub> O <sub>3</sub> 1.8 Al <sub>2</sub> O <sub>3</sub>	75.3	12	<0.5	730		4.	4.5	520
Sa I	5a I 3MgO 2 Al <sub>2</sub> O <sub>3</sub>	75	0	<0.5	820	in H <sub>2</sub> SO <sub>4</sub> , 60°C	0.1	0.1	750
Sb C	5b C 3MgO 2 Al <sub>2</sub> O <sub>3</sub>	45	0	<0.5	730		0.3	0.45	630

C = comparative example; I = example according to the invention 2a mass loss on sintering = 1.6%; 2b mass loss on sintering = 0.2% x in the grain boundary phase

Discussion of the results:

The material described in EP-A 649 824 was reproduced in Example 1 without controlling the oxygen content and, under our conditions, displays a mass loss of 8.5 mg/cm<sup>2</sup>. Setting the SiO<sub>2</sub> content leads to an improvement in the corrosion performance of nominally identical materials by a factor of 30 (as demonstrated by Examples 1a and 1b). The importance of controlling the oxygen content not only in preparation of the mix is shown by comparison of Example 2a with Examples 2b and 2c. While sintering of the material in Example 2a leads to a high weight loss which drastically reduces the SiO<sub>2</sub> content of the sintered material, specimens which were sintered under controlled conditions and have a small weight loss (2b and 2c) display the favourable corrosion performance sought.

It is found that the high  ${\rm SiO_2}$  content leads to a change in the corrosion kinetics. While conventional materials have a linear relationship between corrosion layer thickness and reaction time up to corrosion layer thicknesses of several 100  $\mu m$ , in the case of the materials of the invention, passivation occurs after only a few  $\mu m$  reaction depth (Fig. 2). This passivation occurs all the more quickly, the lower the additive content and the lower the grain size of the silicon nitride grains in the material.

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#### **Claims**

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- 1. Silicon nitride materials containing sintering aids and SiO<sub>2</sub>, characterized in that the molar ratio of the silicon dioxide in the grain boundary phase to the sintering additives including SiO<sub>2</sub> in the grain boundary phase is >60% and the oxide nitride content <1%.
- 2. Process for producing silicon nitride materials according to Claim 1, characterized in that, either alone or in combination,
  - a) the Si<sub>3</sub>N<sub>4</sub> powder used, either alone or together with the sintering aids, is thermally oxidized,
  - b) the Si<sub>3</sub>N<sub>4</sub> powder, either alone or together with the sintering aids and, if desired, further additives, is tribooxidized during milling and/or
  - c) the Si<sub>3</sub>N<sub>4</sub> powder is admixed with sintering aids or with SiO<sub>2</sub> or at least one SiO<sub>2</sub>-forming component either before or during milling.
- 20 3. Use of the silicon nitride materials according to Claim 1 in the construction of machinery and apparatus, in particular in bearings.

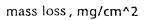
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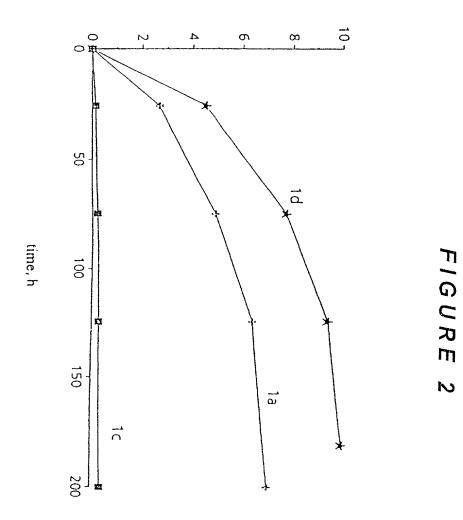
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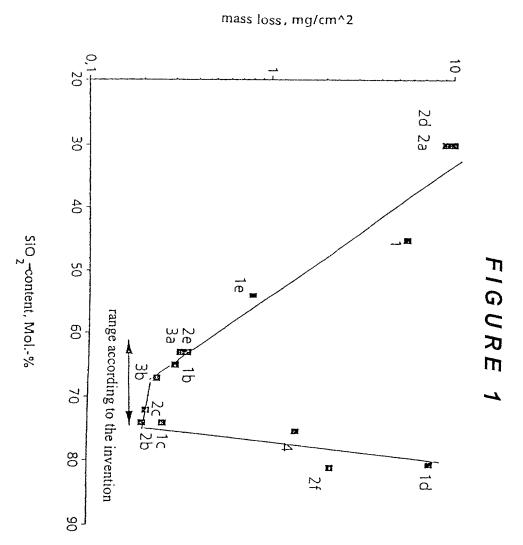
# SILICON NITRIDE SUBSTANCES CONTAINING SINTERING ADDITIVES AND $\mathrm{SiO}_2$ , METHOD FOR PRODUCING THEM AND USE OF THE SAME

# ABSTRACT OF THE DISCLOSURE

The invention relates to silicon nitride substances containing sintering additives and SiO<sub>2</sub>, a method for producing them and the use of the same.







As a below named inventor, I hereby declare that:

My residence, post office address and citizenship are as stated below next to my name. I believe I am the original, first and sole inventor (if only one name is listed below) or an original, first and joint inventor (if plural names are listed below) of the subject matter which is claimed and for which a patent is sought

on the invention entitled

# SILICON NITRIDE SUBSTANCES CONTAINING SINTERING ADDITIVES AND SiO $_{\it 1}$ , $_{\it 2}$ , $_{\it 3}$ FOR PRODUCING THEM AND USE OF THE SAME

METHOD

the specification of which is attached hereto,

or was filed on October 7, 1998

as a PCT Application Serial No. PCT/EP98/06375

I hereby state that I have reviewed and understand the contents of the above-identified specification, including the claims.

I acknowledge the duty to disclose information which is material to the patentability of this application in accordance with Title 37, Code of Federal Regulations, §1.56.

I hereby claim foreign priority benefits under Title 35, United States Code, \$119 of any foreign application(s) for patent or inventor's certificate listed below and have also identified below any foreign application for patent or inventor's certificate having a filing date before that of the application on which priority is claimed:

Prior Foreign Application(s), the priority(ies) of which is/are to be claimed:

197 46 008.9 (Number)

Germany (Country)

October 20, 1997 (Month/Day/Year Filed)

I hereby claim the benefit under Title 35, United States Code, \$120 of any United States application(s) listed below and, insofar as the subject matter of each of the claims of this application is not disclosed in the prior United States application in the manner provided by the first paragraph of Title 35, United States Code, \$112, I acknowledge the duty to disclose the material information as defined in Title 37, Code of Federal Regulations, \$1.56 which occured between the filing date of the prior application and the national or PCT international filing date of this application:

(Application Serial No.)	(Filing Date)	(Status) (patented, pending, abandoned)
(Application Serial No.)	(Filing Date)	(Status)

I hereby declare that all statements made herein of my own knowledge are true and that all statements made on information and belief are believed to be true; and further that these statements were made with the knowledge that willful false statements and the like so made are punishable by fine or imprisonment, or both, under Section 1001 of Title 18 of the United States Code and that such willful false statements may jeopardize the validity of the application or any patent issued thereon.

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